





Hilti HIT-HY 200 mortar with HIT-Z rod

| Injection mortar system | Benefits |
|---|---|
|  <p>Hilti HIT-HY 200-A 500 ml foil pack (also available as 330 ml foil pack)</p> | <ul style="list-style-type: none"> - SAFEset technology: drilling and installing the HIT-Z rod without borehole cleaning - unmatched seismic performance with the highest ETA C1 and C2 approvals - maximum load performance in cracked concrete and uncracked concrete - suitable for cracked and non-cracked concrete C 20/25 to C 50/60 - suitable for use with diamond cored holes in non-cracked or cracked concrete with no load reductions - two mortar (Hilti HIT-HY 200-A and Hilti HIT-HY 200-R) versions available with different curing times and same performance |
|  <p>Hilti HIT-HY 200-R 500 ml foil pack (also available as 330 ml foil pack)</p> | |
|  <p>Static mixer</p> | |
|  <p>HIT-Z HIT-Z-R rod</p> | |



Concrete



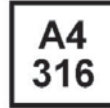
Tensile zone



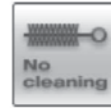
Seismic
ETA-
C1/C2



Fire
resistance



Corrosion
resistance



No cleaning
required for
approved
loads

SAFEset

Hilti
SAFEset
technology
with HIT-Z
rod



European
Technical
Approval



CE
conformity



PROFIS
Anchor
design
software

Approvals / certificates

| Description | Authority / Laboratory | No. / date of issue |
|---|------------------------|--|
| European technical approval ^{a)} | DIBt, Berlin | ETA-12/0006 / 2013-03-15 (HIT-HY 200-A) ETA-12/0028 / 2013-03-15 (HIT-HY 200-R) |
| Fire test report | IBMB, Brunswick | 3501/676/13 / 2012-08-03 |

a) All data given in this section according ETA-12/0006 and ETA-12/0028, issue 2013-03-15.

Basic loading data (for a single anchor)

All data in this section applies to

For details see Simplified design method

- Correct setting (See setting instruction)
- No edge distance and spacing influence
- *Steel* failure
- Base material thickness, as specified in the table
- Embedment depth, as specified in the table
- One anchor material, as specified in the tables
- Concrete C 20/25, $f_{ck,cube} = 25 \text{ N/mm}^2$
- Temperature range I
(min. base material temperature -40°C , max. long term/short term base material temperature: $+24^\circ\text{C}/40^\circ\text{C}$)
- Installation temperature range $+5^\circ\text{C}$ to $+40^\circ\text{C}$

Embedment depth and base material thickness for the basic loading data. Mean ultimate resistance, characteristic resistance, design resistance, recommended loads.

| Anchor size | M8 | M10 | M12 | M16 | M20 |
|------------------------------|-----|-----|-----|-----|-----|
| Typical embedment depth [mm] | 70 | 90 | 110 | 145 | 180 |
| Base material thickness [mm] | 130 | 150 | 170 | 245 | 280 |

Mean ultimate resistance: concrete C 20/25 – $f_{ck,cube} = 25 \text{ N/mm}^2$, element HIT-Z

| Anchor size | M8 | M10 | M12 | M16 | M20 |
|-------------------------------|------|------|------|-------|-------|
| Non-cracked concrete | | | | | |
| Tensile $N_{Ru,m}$ HIT-Z [kN] | 25,2 | 39,9 | 57,8 | 100,8 | 153,3 |
| Shear $V_{Ru,m}$ HIT-Z [kN] | 12,6 | 20,0 | 28,4 | 50,4 | 76,7 |
| Cracked concrete | | | | | |
| Tensile $N_{Ru,m}$ HIT-Z [kN] | 25,2 | 39,9 | 55,1 | 83,4 | 115,4 |
| Shear $V_{Ru,m}$ HIT-Z [kN] | 12,6 | 20,0 | 28,4 | 50,4 | 76,7 |

Characteristic resistance: concrete C 20/25 – $f_{ck,cube} = 25 \text{ N/mm}^2$, element HIT-Z

| Anchor size | M8 | M10 | M12 | M16 | M20 |
|-----------------------------|------|------|------|------|-------|
| Non-cracked concrete | | | | | |
| Tensile N_{Rk} HIT-Z [kN] | 24,0 | 38,0 | 54,3 | 88,2 | 122,0 |
| Shear V_{Rk} HIT-Z [kN] | 12,0 | 19,0 | 27,0 | 48,0 | 73,0 |
| Cracked concrete | | | | | |
| Tensile N_{Rk} HIT-Z [kN] | 21,1 | 30,7 | 41,5 | 62,9 | 86,9 |
| Shear V_{Rk} HIT-Z [kN] | 12,0 | 19,0 | 27,0 | 48,0 | 73,0 |

Design resistance: concrete C 20/25 – $f_{ck,cube} = 25 \text{ N/mm}^2$, element HIT-Z

| Anchor size | M8 | M10 | M12 | M16 | M20 |
|-----------------------------|------|------|------|------|------|
| Non-cracked concrete | | | | | |
| Tensile N_{Rd} HIT-Z [kN] | 16,0 | 25,3 | 36,2 | 58,8 | 81,3 |
| Shear V_{Rd} HIT-Z [kN] | 9,6 | 15,2 | 21,6 | 38,4 | 58,4 |
| Cracked concrete | | | | | |
| Tensile N_{Rd} HIT-Z [kN] | 14,1 | 20,5 | 27,7 | 41,9 | 58,0 |
| Shear V_{Rd} HIT-Z [kN] | 9,6 | 15,2 | 21,6 | 38,4 | 58,4 |

Recommended loads ^{a)}: concrete C 20/25 – $f_{ck,cube} = 25 \text{ N/mm}^2$, element HIT-Z

| Anchor size | | | M8 | M10 | M12 | M16 | M20 |
|----------------------|-------|------|------|------|------|------|------|
| Non-cracked concrete | | | | | | | |
| Tensile N_{rec} | HIT-Z | [kN] | 11,4 | 18,1 | 25,9 | 42,0 | 58,1 |
| Shear V_{rec} | HIT-Z | [kN] | 6,9 | 10,9 | 15,4 | 27,4 | 41,7 |
| Cracked concrete | | | | | | | |
| Tensile N_{rec} | HIT-Z | [kN] | 10,0 | 14,6 | 19,8 | 29,9 | 41,4 |
| Shear V_{rec} | HIT-Z | [kN] | 6,9 | 10,9 | 15,4 | 27,4 | 41,7 |

a) With overall partial safety factor for action $\gamma = 1,4$. The partial safety factors for action depend on the type of loading and shall be taken from national regulations.

Service temperature range

Hilti HIT-HY 200 injection mortar with anchor rod HIT-Z may be applied in the temperature ranges given below. An elevated base material temperature leads to a reduction of the design bond resistance.

| Temperature range | Base material temperature | Maximum long term base material temperature | Maximum short term base material temperature |
|-----------------------|---------------------------|---|--|
| Temperature range I | -40 °C to +40 °C | +24 °C | +40 °C |
| Temperature range II | -40 °C to +80 °C | +40 °C | +80 °C |
| Temperature range III | -40 °C to +120 °C | +72 °C | +120 °C |

Max short term base material temperature

Short-term elevated base material temperatures are those that occur over brief intervals, e.g. as a result of diurnal cycling.

Max long term base material temperature

Long-term elevated base material temperatures are roughly constant over significant periods of time.

Materials
Mechanical properties of HIT-Z and HIT-Z-R

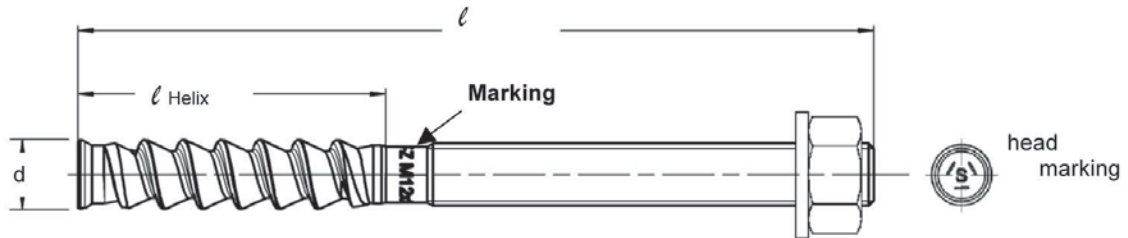
| Anchor size | | | M8 | M10 | M12 | M16 | M20 |
|--|---------|----------------------|------|------|-------|-----|-----|
| Nominal tensile strength f_{uk} | HIT-Z | [N/mm ²] | 650 | 650 | 650 | 610 | 595 |
| | HIT-Z-R | | | | | | |
| Yield strength f_{yk} | HIT-Z | [N/mm ²] | 520 | 520 | 520 | 490 | 480 |
| | HIT-Z-R | | | | | | |
| Stressed cross-section of thread A_s | HIT-Z | [mm ²] | 36,6 | 58,0 | 84,3 | 157 | 245 |
| Moment of resistance W | HIT-Z | [mm ³] | 31,9 | 62,5 | 109,7 | 278 | 542 |

Material quality

| Part | Material |
|---------|---|
| HIT-Z | C-steel cold formed, steel galvanized $\geq 5\mu\text{m}$ |
| HIT-Z-R | stainless steel cold formed, A4 |

Anchor dimensions

| Anchor size | | | M8 | M10 | M12 | M16 | M20 |
|------------------|-----------------------|------|-----|-----|-----|-----|-----|
| Length of anchor | min ℓ | [mm] | 80 | 95 | 105 | 155 | 215 |
| | max ℓ | [mm] | 120 | 160 | 196 | 240 | 250 |
| Helix length | ℓ_{Helix} | [mm] | 50 | 60 | 60 | 96 | 100 |



Installation equipment

| Anchor size | M8 | M10 | M12 | M16 | M20 |
|---------------|--------------|-----|-----|---------------|-----|
| Rotary hammer | TE 2 – TE 40 | | | TE 40 - TE 70 | |

Curing and working time

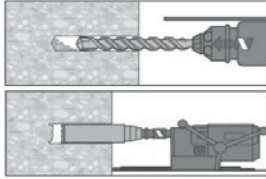
| Temperature of the base material | HIT-HY 200-R | |
|----------------------------------|---|---|
| | Working time in which anchor can be inserted and adjusted t_{work} | Curing time before anchor can be loaded t_{cure} |
| 5 °C | 1 hour | 4 hour |
| 6 °C to 10 °C | 40 min | 2,5 hour |
| 11 °C to 20 °C | 15 min | 1,5 hour |
| 21 °C to 30 °C | 9 min | 1 hour |
| 31 °C to 40 °C | 6 min | 1 hour |

Curing and working time

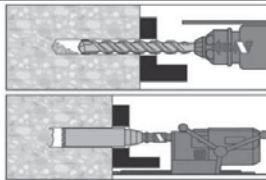
| Temperature of the base material | HIT-HY 200-A | |
|----------------------------------|---|---|
| | Working time in which anchor can be inserted and adjusted t_{work} | Curing time before anchor can be loaded t_{cure} |
| 5 °C | 25 min | 2 hour |
| 6 °C to 10 °C | 15 min | 75 min |
| 11 °C to 20 °C | 7 min | 45 min |
| 21 °C to 30 °C | 4 min | 30 min |
| 31 °C to 40 °C | 3 min | 30 min |

Setting instruction

Bore hole drilling



Pre-setting: Drill hole to the required drilling depth with a hammer drill set in rotation-hammer mode using an appropriately sized carbide drill bit. Diamond coring is permissible when diamond core drilling machine and the corresponding core bit are used.



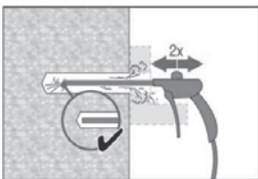
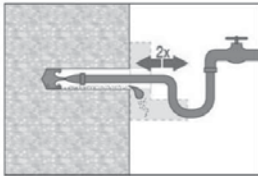
Through-setting: Drill hole through the clearance hole in the fixture to the required drilling depth with a hammer drill set in rotation-hammer mode using an appropriately sized carbide drill bit. Diamond coring is permissible when diamond core drilling machine and the corresponding core bit are used.

Bore hole cleaning^{a)}

a) No cleaning required for hammer drilled boreholes

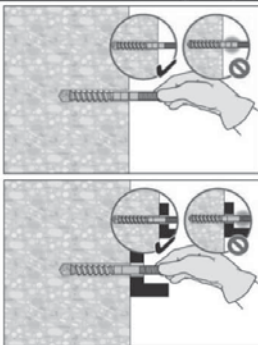
b) Hole flushing and evacuation for wet-drilled diamond cored holes or flooded holes

Flush 2 times from the back of the hole over the hole length.



Blow 2 times the hole with oil-free compressed air (min. 6 bar at 6 m³/h) to evacuate the water

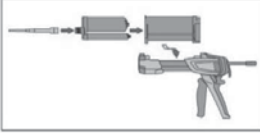
Check of setting depth and compress of the drilling dust



Mark the element and check the setting depth and compress the drilling dust. The element has to fit in the hole until the required embedment depth. If it is not possible to compress the dust, remove the dust in the drill hole or drill deeper.

- a) When drilling downward with non-cleaning the required drilling depths can vary due to accumulation of dust in the hole.

Injection preparation



Tightly attach new Hilti mixing nozzle HIT-RE-M to foil pack manifold (snug fit). Do not modify the mixing nozzle. Observe the instruction for use of the dispenser.

Check foil pack holder for proper function. Do not use damaged foil packs / holders. Swing foil pack holder with foil pack into HIT-dispenser.

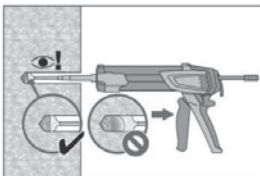


Discard initial adhesive. The foil pack opens automatically as dispensing is initiated. Depending on the size of the foil pack an initial amount of adhesive has to be discarded.

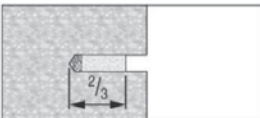
Discard quantities are

| | |
|-----------|----------------------|
| 2 strokes | for 330 ml foil pack |
| 3 strokes | for 500 ml foil pack |

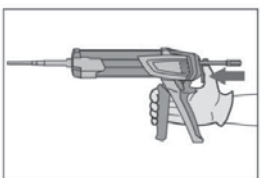
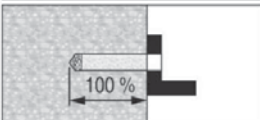
Inject adhesive from the back of the borehole without forming air voids



Inject the adhesive starting at the back of the hole, slowly withdrawing the mixer with each trigger pull.

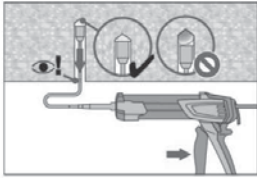


Fill holes approximately 2/3 full for Pre-setting and 100% full for through-setting, or as required to ensure that the annular gap between the anchor and the concrete is completely filled with adhesive along the embedment length.



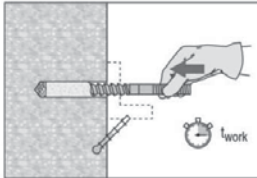
After injection is completed, depressurize the dispenser by pressing the release trigger. This will prevent further adhesive discharge from the mixer.

Overhead installation



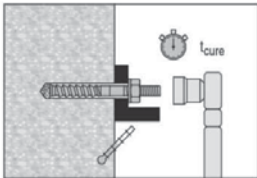
For overhead installation the injection is only possible with the aid of extensions and piston plugs. Assemble HIT-RE-M mixer, extension(s) and appropriately piston plug HIT-SZ. Insert piston plug to back of the hole and inject adhesive. During injection the piston plug will be naturally extruded out of the bore hole by the adhesive pressure

Setting the element



Before use, verify that the element is dry and free of oil and other contaminants. Set element to the required embedment depth until working time t_{work} has elapsed.

After setting the element the annular gap between the anchor and the fixture (through-setting) or concrete (pre-setting) has to be completely filled with mortar.



After required curing time t_{cure} remove excess mortar.

Apply indicated torque moment to activate anchor functioning principles. The anchor can be loaded.

For detailed information on installation see instruction for use given with the package of the product.

Setting details

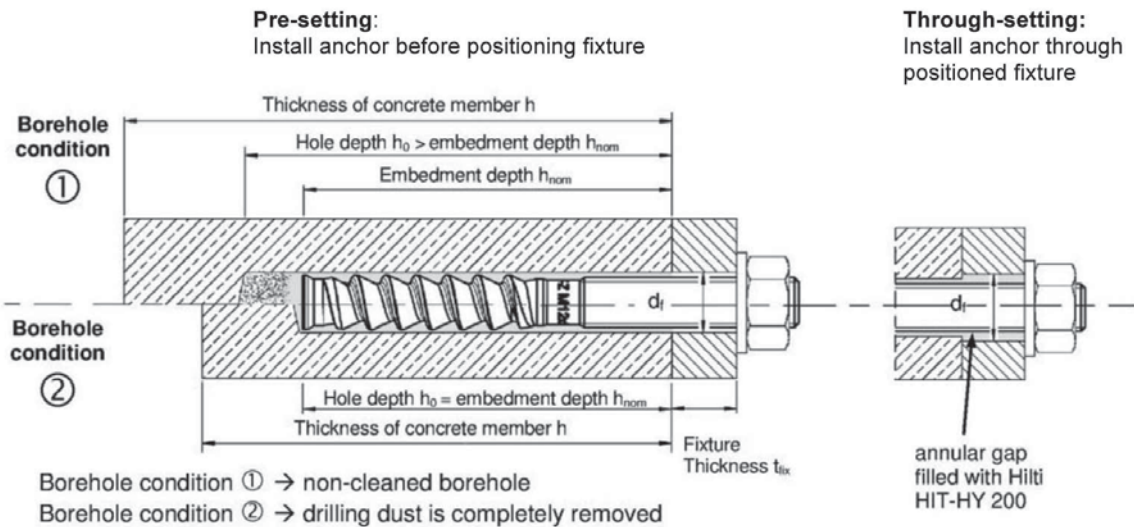
| Anchor size | | M8 | M10 | M12 | M16 | M20 |
|---|--------------------|------------------------------------|-----|-----|-----------------------------------|-----|
| Nominal diameter of drill bit | d_0 [mm] | 10 | 12 | 14 | 18 | 22 |
| Nominal embedment depth range | $h_{nom,min}$ [mm] | 60 | 60 | 60 | 96 | 100 |
| | $h_{nom,max}$ [mm] | 100 | 120 | 150 | 200 | 220 |
| Borehole condition 1 Minimum base material thickness | h_{min} [mm] | $h_{nom} + 60$ mm | | | $h_{nom} + 100$ mm | |
| Borehole condition 2 Minimum base material thickness | h_{min} [mm] | $h_{nom} + 30$ mm ≥ 100 mm | | | $h_{nom} + 45$ mm ≥ 45 mm | |
| Pre-setting: Diameter of clearance hole in the fixture | $d_f \leq$ [mm] | 9 | 12 | 14 | 18 | 22 |
| Through-setting: Diameter of clearance hole in the fixture | $d_f \leq$ [mm] | 11 | 14 | 16 | 20 | 24 |
| Torque moment | T_{inst} [Nm] | 10 | 25 | 40 | 80 | 150 |

Critical edge distance and critical spacing

| | | |
|--|------------------|---|
| Critical spacing for splitting failure | $s_{cr,sp}$ [mm] | $2 c_{cr,sp}$ |
| Critical edge distance for splitting failure | $c_{cr,sp}$ [mm] | $1,5 \cdot h_{nom}$ for $h / h_{nom} \geq 2,35$ |
| | | $6,2 h_{nom} - 2,0 h$ for $2,35 > h / h_{nom} > 1,35$ |
| | | $3,5 h_{nom}$ for $h / h_{nom} \leq 1,35$ |
| Critical spacing for concrete cone failure | $s_{cr,N}$ [mm] | $2 c_{cr,N}$ |
| Critical edge distance for concrete cone failure | $c_{cr,N}$ [mm] | $1,5 h_{nom}$ |

For spacing (or edge distance) smaller than critical spacing (or critical edge distance) the design loads have to be reduced.

a) Embedment depth range: $h_{nom,min} \leq h_{nom} \leq h_{nom,max}$



Minimum edge distance and spacing

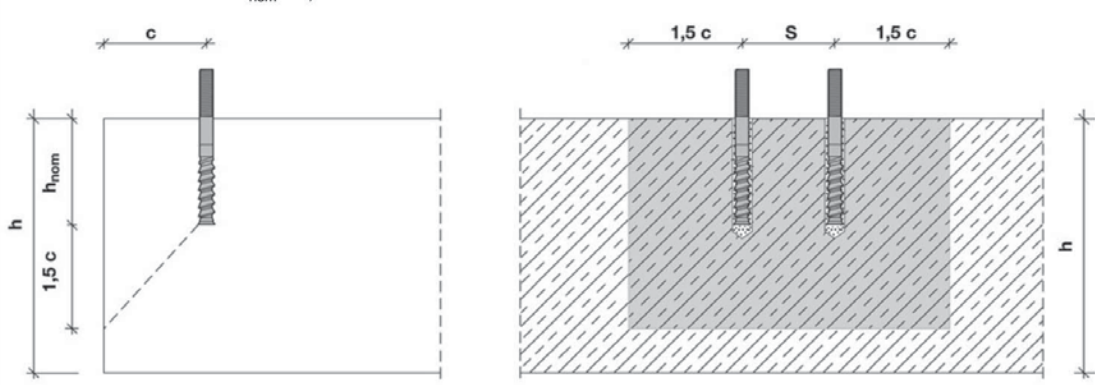
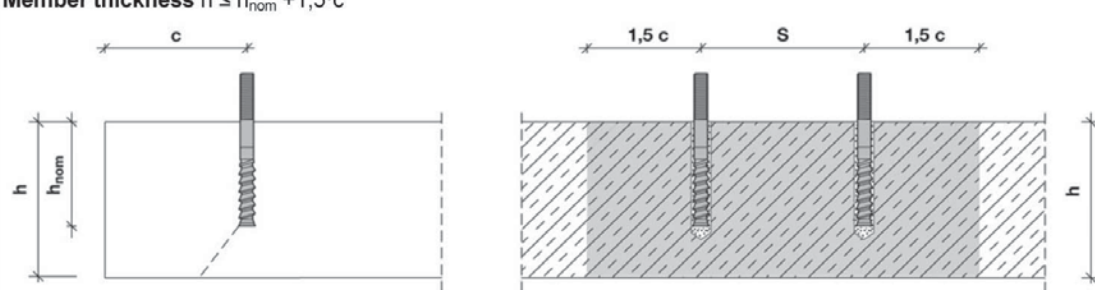
For the calculation of minimum spacing and minimum edge distance of anchors in combination with different embedment depth and thickness of concrete member the following equation shall be fulfilled:

$$A_{i,req} < A_{i,cal}$$

Required interaction area $A_{i,req}$

| Anchor size | | M8 | M10 | M12 | M16 | M20 |
|--------------------|--------------------|-------|-------|-------|--------|--------|
| Cracked concrete | [mm ²] | 19200 | 40800 | 58800 | 94700 | 148000 |
| Uncracked concrete | [mm ²] | 22200 | 57400 | 80800 | 128000 | 198000 |

Calculate interaction area $A_{i,cal}$

| | | | |
|---|--------------------|---|--|
| <p>Member thickness $h \geq h_{nom} + 1,5 \cdot c$</p>  | | | |
| Single anchor and group of anchors with $s > 3 \cdot c$ | [mm ²] | $A_{i,cal} = (6 \cdot c) \cdot (h_{nom} + 1,5 \cdot c)$ | with $c \geq 5 \cdot d$ |
| Group of anchors with $s \leq 3 \cdot c$ | [mm ²] | $A_{i,cal} = (3 \cdot c + s) \cdot (h_{nom} + 1,5 \cdot c)$ | with $c \geq 5 \cdot d$ and $s \geq 5 \cdot d$ |
| <p>Member thickness $h \leq h_{nom} + 1,5 \cdot c$</p>  | | | |
| Single anchor and group of anchors with $s > 3 \cdot c$ | [mm ²] | $A_{i,cal} = (6 \cdot c) \cdot h$ | with $c \geq 5 \cdot d$ |
| Group of anchors with $s \leq 3 \cdot c$ | [mm ²] | $A_{i,cal} = (3 \cdot c + s) \cdot h$ | with $c \geq 5 \cdot d$ and $s \geq 5 \cdot d$ |

**Best case minimum edge distance and spacing
with required member thickness and embedment depth**

| Anchor size | | M8 | M10 | M12 | M16 | M20 |
|-----------------------------|---------------------|-----|-----|-----|-----|-----|
| Cracked concrete | | | | | | |
| Member thickness | $h \geq$ [mm] | 140 | 200 | 240 | 300 | 370 |
| Embedment depth | $h_{nom} \geq$ [mm] | 80 | 120 | 150 | 200 | 220 |
| Minimum spacing | s_{min} [mm] | 40 | 50 | 60 | 80 | 100 |
| Corresponding edge distance | $c \geq$ [mm] | 40 | 55 | 65 | 80 | 100 |
| Minimum edge distance | $c_{min} =$ [mm] | 40 | 50 | 60 | 80 | 100 |
| Corresponding spacing | $s \geq$ [mm] | 40 | 60 | 65 | 80 | 100 |
| Non cracked concrete | | | | | | |
| Member thickness | $h \geq$ [mm] | 140 | 230 | 270 | 340 | 410 |
| Embedment depth | $h_{nom} \geq$ [mm] | 80 | 120 | 150 | 200 | 220 |
| Minimum spacing | s_{min} [mm] | 40 | 50 | 60 | 80 | 100 |
| Corresponding edge distance | $c \geq$ [mm] | 40 | 70 | 80 | 100 | 130 |
| Minimum edge distance | c_{min} [mm] | 40 | 50 | 60 | 80 | 100 |
| Corresponding spacing | $s \geq$ [mm] | 40 | 145 | 160 | 160 | 235 |

**Best case minimum member thickness and embedment depth
with required minimum edge distance and spacing (borehole condition 1)**

| Anchor size | | M8 | M10 | M12 | M16 | M20 |
|-----------------------------|--------------------|-----|-----|-----|-----|-----|
| Cracked concrete | | | | | | |
| Member thickness | h_{min} [mm] | 120 | 120 | 120 | 196 | 200 |
| Embedment depth | $h_{nom,min}$ [mm] | 60 | 60 | 60 | 96 | 100 |
| Minimum spacing | s_{min} [mm] | 40 | 50 | 60 | 80 | 100 |
| Corresponding edge distance | $c \geq$ [mm] | 40 | 100 | 140 | 135 | 215 |
| Minimum edge distance | $c_{min} =$ [mm] | 40 | 60 | 90 | 80 | 125 |
| Corresponding spacing | $s \geq$ [mm] | 40 | 160 | 220 | 235 | 365 |
| Non cracked concrete | | | | | | |
| Member thickness | h_{min} [mm] | 120 | 120 | 120 | 196 | 200 |
| Embedment depth | $h_{nom,min}$ [mm] | 60 | 60 | 60 | 96 | 100 |
| Minimum spacing | s_{min} [mm] | 40 | 50 | 60 | 80 | 100 |
| Corresponding edge distance | $c \geq$ [mm] | 50 | 145 | 200 | 190 | 300 |
| Minimum edge distance | c_{min} [mm] | 40 | 80 | 115 | 110 | 165 |
| Corresponding spacing | $s \geq$ [mm] | 65 | 240 | 330 | 310 | 495 |

Minimum edge distance and spacing – Explanation

Minimum edge and spacing geometrical requirements are determined by testing the installation conditions in which two anchors with a given spacing can be set close to an edge without forming a crack in the concrete due to tightening torque.

The HIT-Z boundary conditions for edge and spacing geometry can be found in the tables to the left. If the embedment depth and slab thickness are equal to or greater than the values in the table, then the edge and spacing values may be utilized.

PROFIS Anchor software is programmed to calculate the referenced equations in order to determine the optimized related minimum edge and spacing based on the following variables:

| | |
|---|--|
| Cracked or uncracked concrete | For cracked concrete it is assumed that a reinforcement is present which limits the crack width to 0,3 mm, allowing smaller values for minimum edge distance and minimum spacing |
| Anchor diameter | For smaller anchor diameter a smaller installation torque is required, allowing smaller values for minimum edge distance and minimum spacing |
| Slab thickness and embedment depth | Increasing these values allows smaller values for minimum edge distance and minimum spacing |

Simplified design method

Simplified version of the design method according ETAG 001, TR 029. Design resistance according data given in ETA-12/0006 (HIT-HY 200-A) and ETA-12/0028 (HIT-HY 200-R) issued on 2013-03-15

- Influence of concrete strength
- Influence of edge distance
- Influence of spacing
- Valid for a group of two anchors. (The method may also be applied for anchor groups with more than two anchors or more than one edge distance. The influencing factors must then be considered for each edge distance and spacing. The simplified calculated design loads take a conservative approach: They will be lower than the exact values according to ETAG 001, TR 029. For an optimized design, anchor calculation can be performed using PROFIS anchor design software.

The design method is based on the following simplification:

- No different loads are acting on individual anchors (no eccentricity)

The values are valid for one anchor.

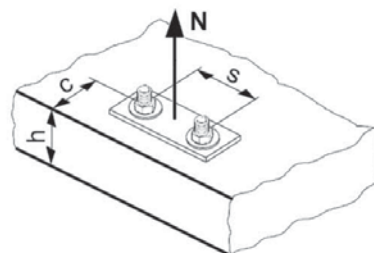
For more complex fastening applications please use the anchor design software PROFIS Anchor.

Tension loading

The design tensile resistance is the lower value of

- Steel resistance: $N_{Rd,s}$
- Combined pull-out and concrete cone resistance: $N_{Rd,p}$
- Concrete cone resistance: $N_{Rd,c} = N_{Rd,c}^0 \cdot f_B \cdot f_{1,N} \cdot f_{2,N} \cdot f_{3,N} \cdot f_{h,N} \cdot f_{re,N}$
- Concrete splitting resistance (only non-cracked concrete): $N_{Rd,sp} = N_{Rd,c}^0 \cdot f_B \cdot f_{1,sp} \cdot f_{2,sp} \cdot f_{3,sp} \cdot f_{h,N}$

$f_{re,N}$



Basic design tensile resistance

Design steel resistance $N_{Rd,s}$

| Anchor size | | M8 | M10 | M12 | M16 | M20 |
|-------------|----------------------|------|------|------|------|------|
| $N_{Rd,s}$ | HIT-Z / HIT-Z-R [kN] | 16,0 | 25,3 | 36,7 | 64,0 | 97,3 |

Design combined pull-out and concrete cone resistance $N_{Rd,p}$ ^{a)}

| Anchor size | | M8 | M10 | M12 | M16 | M20 |
|----------------------|----------------------------|------|------|------|------|-------|
| Non-cracked concrete | | | | | | |
| $N_{Rd,p}^0$ | Temperature range I [kN] | 20,1 | 30,2 | 36,2 | 77,2 | 100,5 |
| $N_{Rd,p}^0$ | Temperature range II [kN] | 18,4 | 27,6 | 33,2 | 70,8 | 92,2 |
| $N_{Rd,p}^0$ | Temperature range III [kN] | 16,8 | 25,1 | 30,2 | 64,3 | 83,8 |
| Cracked concrete | | | | | | |
| $N_{Rd,p}^0$ | Temperature range I [kN] | 18,4 | 27,6 | 33,2 | 70,8 | 92,2 |
| $N_{Rd,p}^0$ | Temperature range II [kN] | 16,8 | 25,1 | 30,2 | 64,3 | 83,8 |
| $N_{Rd,p}^0$ | Temperature range III [kN] | 15,1 | 22,6 | 27,1 | 57,9 | 75,4 |

a) The combined pull-out and concrete cone resistance is independent from the embedment depth.

Design concrete cone resistance $N_{Rd,c} = N_{Rd,c}^0 \cdot f_B \cdot f_{1,N} \cdot f_{2,N} \cdot f_{3,N} \cdot f_{h,N} \cdot f_{re,N}$

Design splitting resistance ^{a)} $N_{Rd,sp} = N_{Rd,c}^0 \cdot f_B \cdot f_{1,sp} \cdot f_{2,sp} \cdot f_{3,sp} \cdot f_{h,N} \cdot f_{re,N}$

| Anchor size | | M8 | M10 | M12 | M16 | M20 |
|--|--|------|------|------|------|------|
| $h_{nom,typ}$ [mm] | | 70 | 90 | 110 | 145 | 180 |
| $N_{Rd,c}^0$ Non cracked concrete [kN] | | 19,7 | 28,7 | 38,8 | 58,8 | 81,3 |
| $N_{Rd,c}^0$ Cracked concrete [kN] | | 14,1 | 20,5 | 27,7 | 41,9 | 58,0 |

a) Splitting resistance must only be considered for non-cracked concrete.

Influencing factors

Influence of concrete strength on combined pull-out and concrete cone resistance

| Concrete strength designation (ENV 206) | C 20/25 | C 25/30 | C 30/37 | C 35/45 | C 40/50 | C 45/55 | C 50/60 |
|---|---------|---------|---------|---------|---------|---------|---------|
| $f_{B,p} =$ | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 |

Influence of concrete strength on concrete cone resistance

| Concrete strength designation (ENV 206) | C 20/25 | C 25/30 | C 30/37 | C 35/45 | C 40/50 | C 45/55 | C 50/60 |
|--|---------|---------|---------|---------|---------|---------|---------|
| $f_B = (f_{ck,cube}/25N/mm^2)^{0,5}$ ^{a)} | 1 | 1,1 | 1,22 | 1,34 | 1,41 | 1,48 | 1,55 |

a) $f_{ck,cube}$ = concrete compressive strength, measured on cubes with 150 mm side length

Influence of edge distance ^{a)}

| $c/c_{cr,N}$ | 0,1 | 0,2 | 0,3 | 0,4 | 0,5 | 0,6 | 0,7 | 0,8 | 0,9 | 1 |
|---|------|------|------|------|------|------|------|------|------|---|
| $c/c_{cr,sp}$ | | | | | | | | | | |
| $f_{1,N} = 0,7 + 0,3 \cdot c/c_{cr,N} \leq 1$ | 0,73 | 0,76 | 0,79 | 0,82 | 0,85 | 0,88 | 0,91 | 0,94 | 0,97 | 1 |
| $f_{1,sp} = 0,7 + 0,3 \cdot c/c_{cr,sp} \leq 1$ | | | | | | | | | | |
| $f_{2,N} = 0,5 \cdot (1 + c/c_{cr,N}) \leq 1$ | 0,55 | 0,60 | 0,65 | 0,70 | 0,75 | 0,80 | 0,85 | 0,90 | 0,95 | 1 |
| $f_{2,sp} = 0,5 \cdot (1 + c/c_{cr,sp}) \leq 1$ | | | | | | | | | | |

a) The edge distance shall not be smaller than the minimum edge distance c_{min} . These influencing factors must be considered for every edge distance smaller than the critical edge distance.

Influence of anchor spacing ^{a)}

| $s/s_{cr,N}$ | 0,1 | 0,2 | 0,3 | 0,4 | 0,5 | 0,6 | 0,7 | 0,8 | 0,9 | 1 |
|---|------|------|------|------|------|------|------|------|------|---|
| $s/s_{cr,sp}$ | | | | | | | | | | |
| $f_{3,N} = 0,5 \cdot (1 + s/s_{cr,N}) \leq 1$ | 0,55 | 0,60 | 0,65 | 0,70 | 0,75 | 0,80 | 0,85 | 0,90 | 0,95 | 1 |
| $f_{3,sp} = 0,5 \cdot (1 + s/s_{cr,sp}) \leq 1$ | | | | | | | | | | |

a) The anchor spacing shall not be smaller than the minimum anchor spacing s_{min} . This influencing factor must be considered for every anchor spacing.

Influence of embedment depth on concrete cone resistance

$$f_{h,N} = (h_{nom}/h_{nom,typ})^{1,5}$$

Influence of reinforcement

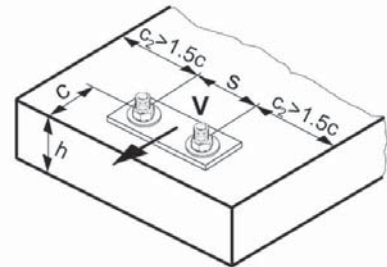
| h_{nom} [mm] | 60 | 70 | 80 | 90 | ≥ 100 |
|---|-------------------|--------------------|-------------------|--------------------|------------|
| $f_{re,N} = 0,5 + h_{nom}/200mm \leq 1$ | 0,8 ^{a)} | 0,85 ^{a)} | 0,9 ^{a)} | 0,95 ^{a)} | 1 |

a) This factor applies only for dense reinforcement. If in the area of anchorage there is reinforcement with a spacing ≥ 150 mm (any diameter) or with a diameter ≤ 10 mm and a spacing ≥ 100 mm, then a factor $f_{re,N} = 1$ may be applied.

Shear loading

The design shear resistance is the lower value of

- Steel resistance: $V_{Rd,s}$
- Concrete pryout resistance: $V_{Rd,cp} = k \cdot \text{lower value of } N_{Rd,p} \text{ and } N_{Rd,c}$
- Concrete edge resistance: $V_{Rd,c} = V_{Rd,c}^0 \cdot f_B \cdot f_h \cdot f_4 \cdot f_{hef} \cdot f_c$



Basic design shear resistance

Design steel resistance $V_{Rd,s}$

| Anchor size | | M8 | M10 | M12 | M16 | M20 |
|--------------------|------|------|------|------|------|------|
| $V_{Rd,s}$ HIT-Z | [kN] | 9,6 | 15,2 | 21,6 | 38,4 | 58,4 |
| $V_{Rd,s}$ HIT-Z-R | [kN] | 11,2 | 18,4 | 26,4 | 45,6 | 70,4 |

Design concrete pryout resistance $V_{Rd,cp} = \text{lower value}^a$ of $k \cdot N_{Rd,p}$ and $k \cdot N_{Rd,c}$

$$k = 2 \text{ for } h_{ef} \geq 60 \text{ mm}$$

- a) $N_{Rd,p}$: Design combined pull-out and concrete cone resistance
 $N_{Rd,c}$: Design concrete cone resistance

Design concrete edge resistance $V_{Rd,c} = V_{Rd,c}^0 \cdot f_B \cdot f_h \cdot f_4$

| Anchor size | | Non-cracked concrete | | | | | Cracked concrete | | | | |
|--------------|------|----------------------|-----|------|------|------|------------------|-----|-----|------|------|
| | | M8 | M10 | M12 | M16 | M20 | M8 | M10 | M12 | M16 | M20 |
| $V_{Rd,c}^0$ | [kN] | 5,8 | 8,6 | 11,6 | 18,9 | 27,4 | 4,1 | 6,0 | 8,2 | 13,3 | 19,4 |

- a) For anchor groups only the anchors close to the edge must be considered.

Influencing factors

Influence of concrete strength

| Concrete strength designation (ENV 206) | C 20/25 | C 25/30 | C 30/37 | C 35/45 | C 40/50 | C 45/55 | C 50/60 |
|--|---------|---------|---------|---------|---------|---------|---------|
| $f_{ck} = (f_{ck,cube}/25N/mm^2)^{1/2}$ a) | 1 | 1,1 | 1,22 | 1,34 | 1,41 | 1,48 | 1,55 |

- a) $f_{ck,cube}$ = concrete compressive strength, measured on cubes with 150 mm side length

Influence of angle between load applied and the direction perpendicular to the free edge

| Angle β | 0° | 10° | 20° | 30° | 40° | 50° | 60° | 70° | 80° | ≥ 90° |
|---|----|------|------|------|------|------|------|------|------|-------|
| $f_{\beta} = \frac{1}{\sqrt{(\cos \alpha_v)^2 + \left(\frac{\sin \alpha_v}{2,5}\right)^2}}$ | 1 | 1,01 | 1,05 | 1,13 | 1,24 | 1,40 | 1,64 | 1,97 | 2,32 | 2,50 |

Influence of base material thickness

| h/c | 0,15 | 0,3 | 0,45 | 0,6 | 0,75 | 0,9 | 1,05 | 1,2 | 1,35 | ≥ 1,5 |
|--|------|------|------|------|------|------|------|------|------|-------|
| $f_h = \{h/(1,5 \cdot c)\}^{1/2} \leq 1$ | 0,32 | 0,45 | 0,55 | 0,63 | 0,71 | 0,77 | 0,84 | 0,89 | 0,95 | 1,00 |

Influence of anchor spacing and edge distance ^{a)} for concrete edge resistance: f_4
 $f_4 = (c/h_{nom})^{1,5} \cdot (1 + s / [3 \cdot c]) \cdot 0,5$

| c/h _{nom} | Single anchor | Group of two anchors s/h _{nom} | | | | | | | | | | | | | | |
|--------------------|---------------|---|------|------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| | | 0,75 | 1,50 | 2,25 | 3,00 | 3,75 | 4,50 | 5,25 | 6,00 | 6,75 | 7,50 | 8,25 | 9,00 | 9,75 | 10,50 | 11,25 |
| 0,50 | 0,35 | 0,27 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 | 0,35 |
| 0,75 | 0,65 | 0,43 | 0,54 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 | 0,65 |
| 1,00 | 1,00 | 0,63 | 0,75 | 0,88 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 | 1,00 |
| 1,25 | 1,40 | 0,84 | 0,98 | 1,12 | 1,26 | 1,40 | 1,40 | 1,40 | 1,40 | 1,40 | 1,40 | 1,40 | 1,40 | 1,40 | 1,40 | 1,40 |
| 1,50 | 1,84 | 1,07 | 1,22 | 1,38 | 1,53 | 1,68 | 1,84 | 1,84 | 1,84 | 1,84 | 1,84 | 1,84 | 1,84 | 1,84 | 1,84 | 1,84 |
| 1,75 | 2,32 | 1,32 | 1,49 | 1,65 | 1,82 | 1,98 | 2,15 | 2,32 | 2,32 | 2,32 | 2,32 | 2,32 | 2,32 | 2,32 | 2,32 | 2,32 |
| 2,00 | 2,83 | 1,59 | 1,77 | 1,94 | 2,12 | 2,30 | 2,47 | 2,65 | 2,83 | 2,83 | 2,83 | 2,83 | 2,83 | 2,83 | 2,83 | 2,83 |
| 2,25 | 3,38 | 1,88 | 2,06 | 2,25 | 2,44 | 2,63 | 2,81 | 3,00 | 3,19 | 3,38 | 3,38 | 3,38 | 3,38 | 3,38 | 3,38 | 3,38 |
| 2,50 | 3,95 | 2,17 | 2,37 | 2,57 | 2,77 | 2,96 | 3,16 | 3,36 | 3,56 | 3,76 | 3,95 | 3,95 | 3,95 | 3,95 | 3,95 | 3,95 |
| 2,75 | 4,56 | 2,49 | 2,69 | 2,90 | 3,11 | 3,32 | 3,52 | 3,73 | 3,94 | 4,15 | 4,35 | 4,56 | 4,56 | 4,56 | 4,56 | 4,56 |
| 3,00 | 5,20 | 2,81 | 3,03 | 3,25 | 3,46 | 3,68 | 3,90 | 4,11 | 4,33 | 4,55 | 4,76 | 4,98 | 5,20 | 5,20 | 5,20 | 5,20 |
| 3,25 | 5,86 | 3,15 | 3,38 | 3,61 | 3,83 | 4,06 | 4,28 | 4,51 | 4,73 | 4,96 | 5,18 | 5,41 | 5,63 | 5,86 | 5,86 | 5,86 |
| 3,50 | 6,55 | 3,51 | 3,74 | 3,98 | 4,21 | 4,44 | 4,68 | 4,91 | 5,14 | 5,38 | 5,61 | 5,85 | 6,08 | 6,31 | 6,55 | 6,55 |
| 3,75 | 7,26 | 3,87 | 4,12 | 4,36 | 4,60 | 4,84 | 5,08 | 5,33 | 5,57 | 5,81 | 6,05 | 6,29 | 6,54 | 6,78 | 7,02 | 7,26 |
| 4,00 | 8,00 | 4,25 | 4,50 | 4,75 | 5,00 | 5,25 | 5,50 | 5,75 | 6,00 | 6,25 | 6,50 | 6,75 | 7,00 | 7,25 | 7,50 | 7,75 |
| 4,25 | 8,76 | 4,64 | 4,90 | 5,15 | 5,41 | 5,67 | 5,93 | 6,18 | 6,44 | 6,70 | 6,96 | 7,22 | 7,47 | 7,73 | 7,99 | 8,25 |
| 4,50 | 9,55 | 5,04 | 5,30 | 5,57 | 5,83 | 6,10 | 6,36 | 6,63 | 6,89 | 7,16 | 7,42 | 7,69 | 7,95 | 8,22 | 8,49 | 8,75 |
| 4,75 | 10,35 | 5,45 | 5,72 | 5,99 | 6,27 | 6,54 | 6,81 | 7,08 | 7,36 | 7,63 | 7,90 | 8,17 | 8,45 | 8,72 | 8,99 | 9,26 |
| 5,00 | 11,18 | 5,87 | 6,15 | 6,43 | 6,71 | 6,99 | 7,27 | 7,55 | 7,83 | 8,11 | 8,39 | 8,66 | 8,94 | 9,22 | 9,50 | 9,78 |
| 5,25 | 12,03 | 6,30 | 6,59 | 6,87 | 7,16 | 7,45 | 7,73 | 8,02 | 8,31 | 8,59 | 8,88 | 9,17 | 9,45 | 9,74 | 10,02 | 10,31 |
| 5,50 | 12,90 | 6,74 | 7,04 | 7,33 | 7,62 | 7,92 | 8,21 | 8,50 | 8,79 | 9,09 | 9,38 | 9,67 | 9,97 | 10,26 | 10,55 | 10,85 |

a) The anchor spacing and the edge distance shall not be smaller than the minimum anchor spacing s_{min} and the minimum edge distance c_{min} .

Influence of embedment depth

| h_{nom}/d | 4 | 4,5 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
|---|------|------|------|------|------|------|------|------|------|
| $f_{hef} = 0,05 \cdot (h_{nom} / d)^{1,68}$ | 0,51 | 0,63 | 0,75 | 1,01 | 1,31 | 1,64 | 2,00 | 2,39 | 2,81 |
| h_{ef}/d | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 |
| $f_{hef} = 0,05 \cdot (h_{nom} / d)^{1,68}$ | 3,25 | 3,72 | 4,21 | 4,73 | 5,27 | 5,84 | 6,42 | 7,04 | 7,67 |

Influence of edge distance ^{a)}

| c/d | 4 | 6 | 8 | 10 | 15 | 20 | 30 | 40 |
|------------------------|------|------|------|------|------|------|------|------|
| $f_c = (d / c)^{0,19}$ | 0,77 | 0,71 | 0,67 | 0,65 | 0,60 | 0,57 | 0,52 | 0,50 |

a) The edge distance shall not be smaller than the minimum edge distance c_{min} .

Combined tension and shear loading

For combined tension and shear loading see section "Anchor Design".

Seismic design C1 and C2

Basic loading data for concrete C20/25 – C50/60

All data in this section applies to:

- Seismic design according to TR045

The following technical data are based on: ETA-12/0006 and ETA-12/0028, issue 2013-03-15

Anchorage depth range

| Anchor size | | M8 | M10 | M12 | M16 | M20 |
|-------------------------------|--------------------|-----|-----|-----|-----|-----|
| Nominal anchorage depth range | $h_{nom,min}$ [mm] | 60 | 60 | 60 | 96 | 100 |
| | $h_{nom,max}$ [mm] | 100 | 120 | 144 | 192 | 220 |

Tension resistance in case of seismic performance category C1

| Anchor size | | M8 | M10 | M12 | M16 | M20 |
|--|--|-----|-----|-----|-----|-----|
| Characteristic tension resistance to steel failure | | | | | | |
| HIT-Z / HIT-Z-R | $N_{Rk,s,seis}$ [kN] | 24 | 38 | 55 | 96 | 146 |
| Partial safety factor | $\gamma_{Ms,seis}$ [-] | 1,5 | | | | |
| Characteristic bond resistance in cracked concrete C20/25 to C50/60 | | | | | | |
| Temperature range I: 24°C/40°C | $\tau_{Rk,seis}$ [N/mm ²] | 21 | | | | |
| Temperature range II: 50°C/80°C | $\tau_{Rk,seis}$ [N/mm ²] | 19 | | | | |
| Temperature range III: 72°C/120°C | $\tau_{Rk,seis}$ [N/mm ²] | 17 | | | | |
| Partial safety factor | $\gamma_{Mp,seis}$ [-] | 1,5 | | | | |
| Concrete cone resistance and splitting resistance | | | | | | |
| Partial safety factor | $\gamma_{Mc,seis} = \gamma_{Msp,seis}$ [-] | 1,5 | | | | |

Displacement under tension load in case of seismic performance category C1¹⁾

| Anchor size | | M8 | M10 | M12 | M16 | M20 |
|--------------------------------|------------------------|-----|-----|-----|-----|-----|
| Displacement (HIT-Z / HIT-Z-R) | $\delta_{N,seis}$ [mm] | 1,2 | 1,9 | 1,7 | 1,3 | 1,8 |

1) Maximum displacement during cycling (seismic event).

Shear resistance in case of seismic performance category C1¹⁾

| Anchor size | | M8 | M10 | M12 | M16 | M20 |
|--|--|------|-----|-----|-----|-----|
| Characteristic shear resistance to steel failure | | | | | | |
| HIT-Z | $V_{Rk,s,seis}$ [kN] | 7 | 17 | 16 | 28 | 45 |
| HIT-Z-R | $V_{Rk,s,seis}$ [kN] | 8 | 19 | 22 | 31 | 48 |
| Partial safety factor | $\gamma_{Ms,seis}$ [-] | 1,25 | | | | |
| Concrete pryout resistance and concrete edge resistance | | | | | | |
| Partial safety factor | $\gamma_{Mcp,seis} = \gamma_{Mc,seis}$ [-] | 1,5 | | | | |

1) Reduction factor $\alpha_{gap} = 1,0$ when using the Hilti Dynamic Set

Displacement under shear load in case of seismic performance category C1¹⁾

| Anchor size | | M8 | M10 | M12 | M16 | M20 |
|------------------------|------------------------|-----|-----|-----|-----|-----|
| Displacement (HIT-Z) | $\delta_{V,seis}$ [mm] | 4,0 | 5,0 | 4,9 | 4,3 | 5,5 |
| Displacement (HIT-Z-R) | $\delta_{V,seis}$ [mm] | 5,0 | 5,6 | 5,9 | 6,0 | 6,4 |

1) Maximum displacement during cycling (seismic event).

Tension resistance in case of seismic performance category C2

| Anchor size | | M12 | M16 |
|--|--|-----|-----|
| Characteristic tension resistance to steel failure | | | |
| HIT-Z / HIT-Z-R | $N_{Rk,s,seis}$ [kN] | 55 | 96 |
| Partial safety factor ¹⁾ | $\gamma_{Ms,seis}$ [-] | 1,5 | |
| Characteristic bond resistance in cracked concrete C20/25 to C50/60 | | | |
| Temperature range I: 24°C/40°C | $\tau_{Rk,s,seis}$ [N/mm ²] | 13 | 19 |
| Temperature range II: 50°C/80°C | $\tau_{Rk,s,seis}$ [N/mm ²] | 12 | 17 |
| Temperature range III: 72°C/120°C | $\tau_{Rk,s,seis}$ [N/mm ²] | 10 | 16 |
| Partial safety factor | $\gamma_{Mp,seis}$ [-] | 1,5 | |
| Concrete cone resistance and splitting resistance | | | |
| Partial safety factor | $\gamma_{Mc,seis} = \gamma_{Msp,seis}$ [-] | 1,5 | |

Displacement under tension load in case of seismic performance category C2

| Anchor size | | M12 | M16 |
|------------------------------------|------------------------|-----|-----|
| Displacement DLS (HIT-Z / HIT-Z-R) | $\delta_{N,seis}$ [mm] | 1,3 | 1,9 |
| Displacement ULS (HIT-Z / HIT-Z-R) | $\delta_{N,seis}$ [mm] | 3,2 | 3,6 |

Shear resistance in case of seismic performance category C2 ¹⁾

| Anchor size | | M12 | M16 |
|--|--|------|-----|
| Characteristic shear resistance to steel failure | | | |
| HIT-Z | $V_{Rk,s,seis}$ [kN] | 11 | 17 |
| HIT-Z-R | $V_{Rk,s,seis}$ [kN] | 16 | 21 |
| Partial safety factor | $\gamma_{Ms,seis}$ [-] | 1,25 | |
| Concrete pryout resistance and concrete edge resistance | | | |
| Partial safety factor | $\gamma_{Mcp,seis} = \gamma_{Mc,seis}$ [-] | 1,5 | |

1) Reduction factor $\alpha_{gap} = 1,0$ when using the Hilti Dynamic Set

Displacement under shear load in case of seismic performance category C2

| Anchor size | | M12 | M16 |
|----------------------------|------------------------|-----|-----|
| Displacement DLS (HIT-Z) | $\delta_{V,seis}$ [mm] | 2,8 | 3,1 |
| Displacement ULS (HIT-Z) | $\delta_{V,seis}$ [mm] | 4,6 | 6,2 |
| Displacement DLS (HIT-Z-R) | $\delta_{V,seis}$ [mm] | 3,0 | 3,1 |
| Displacement ULS (HIT-Z-R) | $\delta_{V,seis}$ [mm] | 6,2 | 6,2 |

For seismic resistant fastening applications please use the anchor design software PROFIS Anchor.

